

On Identification of Distribution Grids

Omid Ardakanian, Ye Yuan, Vincent W.S. Wong, Roel Dobbe,
Steven H. Low, Alexandra von Meier, and Claire Tomlin

Abstract—Large-scale integration of distributed energy resources into distribution feeders necessitates careful control of their operation through power flow analysis. While the knowledge of the distribution system model is crucial for this analysis, it is often unavailable or outdated. The recent introduction of synchrophasor technology in low-voltage distribution grids has created ample opportunity to learn this model from high-precision, time-synchronized measurements of voltage and current phasors at various locations. This paper focuses on joint estimation of admittance parameters and topology of a poly-phase distribution network from the available telemetry data via the lasso, a method for regression shrinkage and selection. We propose tractable convex programs capable of tackling the low rank structure of the distribution system and develop an online algorithm for early detection and localization of critical events that induce a change in the admittance matrix. The efficacy of these techniques to identify a large part of the distribution network is corroborated through power flow analysis on four three-phase radial distribution systems serving real and synthetic household demands.

Index Terms—System identification, event detection, phasor measurement units, distribution grids, smart grids.

I. INTRODUCTION

DISTRIBUTION grids were traditionally sized in a way that they would not be stressed under severe loading conditions. This fit and forget strategy worked well enough for many years owing to the simple design and operation rules of these networks. But the rapid growth in deployment of demand side technologies and distributed energy resources (DER), such as solar panels, wind turbines, battery storage systems, and plug-in electric vehicles, in recent years has led to unprecedented amounts of variability and uncertainty which complicate grid operations and threaten its reliability. This necessitates more comprehensive monitoring of distribution circuits beyond the substation and manifests the need for a novel planning and operation paradigm centered around pervasive monitoring, real-time analytics, and proactive control [1].

Numerous smart grid technologies have been piloted in recent years to make electrical events and responses observable and comparable between multiple locations, examples of which are the distribution supervisory control and data acquisition (D-SCADA) system and distribution-level synchrophasor technology [2] — a network of inexpensive and high-fidelity phasor measurement units (termed μ PMUs) sampling voltage and current waveforms at high frequency [3]. Distribution system operators could use measurements of these sensors

along with appropriate analytical tools for many purposes, including topology detection, model validation, state estimation, distributed generation characterization, fault detection, equipment health monitoring, and phasor-based control [4]–[6]. These capabilities are essential for cost-effective planning and reliable operation of distribution systems.

While only a small number of nodes are currently equipped with μ PMUs, these sensors are expected to become more common in low-voltage distribution grids in the future. Specifically, synchrophasor capability can be built into devices such as inverters, relays, and transformers, which are connected to many nodes in the network. Hence, the synchrophasor network can potentially cover the entire distribution network, including intermediate and end nodes. Assuming that synchrophasor data is available from all nodes, this paper focuses on joint estimation of distribution system model parameters and its topology. The knowledge of the distribution system model is of vital importance for many diagnostics and control applications, yet it is often unavailable or outdated due to the continuous integration of distribution components and frequent reconfiguration of feeders.

The *inverse power flow* (iPF) problem, originally defined in [7], concerns recovering the admittance matrix of a power system from a sequence of voltage and current phasor measurements corresponding to different steady states of the system. In this paper, we study the iPF problem in the context of a poly-phase distribution system (loopy or radial) where each node is equipped with a sensor (i.e., the full observability assumption). Drawing on sparsity-based regularization techniques [8]–[10], we present a tractable convex program to uniquely identify the admittance matrix of the distribution system when the identification problem is well-posed. To tackle the low rank structure of a distribution network, we develop a novel algorithm based on matrix decomposition which is capable of identifying a large submatrix of the admittance matrix. Furthermore, we propose an online algorithm for early detection and localization of critical events that change the admittance matrix in one way or another. Extensive simulations are performed to evaluate the efficacy of these algorithms on IEEE 13, 34, 37, and 123-bus feeders serving real and synthetic loads.

This paper extends our prior work [11] in two main ways. First, we propose the use of the *adaptive lasso* penalty to estimate large elements of the admittance matrix, attenuating the bias problem. Second, we propose a regularization technique that leverages the approximate knowledge of the admittance matrix to enhance identification when the constructed data matrix is low rank. Third, we exploit the parametric sparsity in the difference between the true admittance matrix and the one after event so that one can reduce the number of samples to localize the event.

Omid Ardakanian is with the Department of Computing Science, University of Alberta, Canada. Ye Yuan is with the School of Automation, Huazhong University of Science and Technology, China. Vincent W.S. Wong is with the Department of Electrical and Computer Engineering, University of British Columbia, Canada. Steven H. Low is with the Department of Computing and Mathematical Science, California Institute of Technology, USA. Roel Dobbe, Alexandra von Meier, and Claire Tomlin are with the Department of Electrical Engineering and Computer Sciences, UC Berkeley, USA. (For correspondence: Prof. Ye Yuan, yye@hust.edu.cn.)

II. RELATED WORK

The distribution system identification problem has received a lot of attention lately. However, most research focuses on topology verification which entails identifying the subset of distribution lines that are energized using smart meter data or phasor measurements, and little effort has been put into learning the impedance parameters of lines and transformers from the available sensor data. Due to the imprecise and correlated phasor measurements, model parameter estimation will be nontrivial even if the true topology is known. For example, the correlation between node voltage measurements is leveraged in [12] to detect the grid topology via a sparse Markov random field. Power measurements collected from different types of meters are used in [13] to detect the topology of a radial distribution system by solving an integer programming problem. A data-driven algorithm based on group lasso is proposed in [14] to identify the topology of a mesh distribution network using voltage magnitude and power consumption measurements of smart meters. A data-driven online algorithm is proposed in [15] for detecting a switching event by comparing a trend vector built from μ PMU data with a given library of signatures derived from the possible topology changes. This algorithm cannot be utilized to efficiently detect topology change events in a large distribution network due to the exponential number of feasible radial structures. In [16], the optimal placement of sensors in a distribution network is investigated in order to infer the status of switches from the measurements using the maximum likelihood method. This approach requires the knowledge of the number of switches installed in the network and their location. A mutual information-based algorithm is proposed in [17] to identify the distribution topology by building a graphical model that describes the probabilistic relationship among voltage measurements. In [18], a graphical model learning algorithm is proposed based on conditional independence tests for nodal voltage measurements. Principal component analysis is employed in [19] to obtain a lower dimensional subspace of the available μ PMU data and project the original data onto this subspace by learning coefficients of the basis matrix using an adaptive training method. An online event detection algorithm is then proposed to approximate phasor measurements using these coefficients, issuing an alert whenever a significant approximation error is noticed. While some of these works can accurately identify real-time topology of the distribution network, none of them investigated the system identification (or model parameter estimation) problem in radial or mesh distribution systems.

The closest lines of work to ours are [20], [21] which attempt to jointly address the topology detection and model parameter estimation problems. In [20], these problems are merely studied in a radial setting assuming the true variance of nodal power injection (real and reactive) are known and sensor measurements are precise. We do not make these assumptions in this work. In [21], the maximum likelihood estimation framework is used to jointly estimate the line parameters and topology of a distribution system given noisy measurements of power injections and voltage phasors obtained from μ PMUs and smart meters. Despite the novelty of this work, the authors used a single-phase power flow model, ignoring the mutual coupling between phase conductors. Our approach is different from theirs in two ways. First, we adopt a three-phase ac model

for describing power flow in distribution systems. Second, we address detection and localization of events and faults that could induce a change in the admittance matrix.

We note that the system identification problem studied in this paper is analogous to *network tomography*, which concerns inferring internal performance information and topology of a computer network from measurements [22].

III. PROBLEM FORMULATION

This section describes the iPF problem in a poly-phase distribution system and introduces a regularization technique for simultaneous estimation and variable selection to efficiently solve this problem under certain assumptions.

A. Preliminaries

We denote the set of complex matrices and the set of symmetric complex matrices by \mathbb{C} and \mathbb{S} , respectively, the transpose of a matrix A by A^T , its Hermitian (complex conjugate) transpose by A^H , its pseudo-inverse by A^\dagger , its Frobenius norm by $\|A\|_F$, and the smallest number of linearly dependent columns of this matrix by $\text{Spark}(A)$. All-zeros and all-ones vectors are denoted respectively by $\mathbf{0}$ and $\mathbf{1}$, and the cardinality of a set \mathcal{N} is denoted by $|\mathcal{N}|$. Placing a caret over a letter indicates that it represents an estimated value.

A poly-phase power distribution system can be modeled by an undirected graph $\mathcal{G} = (\mathcal{N}, \mathcal{E})$ where $\mathcal{N} = \{1, 2, \dots, N\}$ represents the set of nodes, and $\mathcal{E} \subseteq \mathcal{N} \times \mathcal{N}$ represents the set of energized lines, each connecting two distinct nodes. We denote the phases of a node $n \in \mathcal{N}$ by $\mathcal{P}_n \subseteq \{a_n, b_n, c_n\}$ and the phases of a line $(m, n) \in \mathcal{E}$ connecting node m to node n by $\mathcal{P}_{mn} \subseteq \{a_{mn}, b_{mn}, c_{mn}\}$. For node $n \in \mathcal{N}$ and phase $\phi \in \mathcal{P}_n$, let $V_n^\phi \in \mathbb{C}$ be its line-to-ground voltage and $I_n^\phi \in \mathbb{C}$ be the injected current. We represent the voltages and injected currents of different phases of node $n \in \mathcal{N}$ by vectors $V_n = \{V_n^\phi\}_{\phi \in \mathcal{P}_n}$ and $I_n = \{I_n^\phi\}_{\phi \in \mathcal{P}_n}$, respectively, and use the per-unit system to express the quantities. We treat the voltage at the distribution substation as reference for phasor representation.

We model lines as π -equivalent components and denote the phase impedance and shunt admittance matrices of line (m, n) by $Z_{mn} \in \mathbb{C}^{|\mathcal{P}_{mn}| \times |\mathcal{P}_{mn}|}$ and $Y_{mn}^s \in \mathbb{C}^{|\mathcal{P}_{mn}| \times |\mathcal{P}_{mn}|}$, respectively. Similarly, transformers are modeled as series components with an admittance matrix which depends on the type of connection. Assembling the admittance matrices of all components, the admittance matrix can be constructed for the distribution system, denoted by $Y_{\text{bus}} \in \mathbb{S}^{\sum_{n \in \mathcal{N}} |\mathcal{P}_n| \times \sum_{n \in \mathcal{N}} |\mathcal{P}_n|}$, which is a symmetric matrix that satisfies $Y_{\text{bus}} \mathbf{1} = \mathbf{0}$ if shunt elements are neglected. The bus admittance matrix relates the node voltages and injected currents according to Ohm's law:

$$\underbrace{\begin{bmatrix} I_1(k) \\ I_2(k) \\ \vdots \\ I_N(k) \end{bmatrix}}_{I_{\text{bus}}(k)} = \underbrace{\begin{bmatrix} Y_{11} & Y_{12} & \dots & Y_{1N} \\ Y_{12}^T & Y_{22} & \dots & Y_{2N} \\ \vdots & \vdots & \ddots & \vdots \\ Y_{1N}^T & Y_{2N}^T & \dots & Y_{NN} \end{bmatrix}}_{Y_{\text{bus}}} \underbrace{\begin{bmatrix} V_1(k) \\ V_2(k) \\ \vdots \\ V_N(k) \end{bmatrix}}_{V_{\text{bus}}(k)}, \quad (1)$$

where $k = 1, \dots, K$ is the time index, $V_{\text{bus}}(k), I_{\text{bus}}(k) \in \mathbb{C}^{\sum_{n \in \mathcal{N}} |\mathcal{P}_n| \times 1}$ are steady-state complex nodal voltages and injected currents at time k , each off-diagonal block of Y_{bus} is a

submatrix $Y_{mn} = -Z_{mn}^{-1}$ corresponding to the admittance of a poly-phase line (m, n) , and each diagonal block is a submatrix

$$Y_{nn} = \sum_{m \in \{o | (o, n) \in \mathcal{E}\}} \left(\frac{1}{2} Y_{mn}^s + Z_{mn}^{-1} \right).$$

Hence, the admittance matrix incorporates the mutual coupling between phase conductors.

Rewriting (1) in vector form for K time slots yields:

$$\underbrace{\begin{bmatrix} I_1(1) & \dots & I_1(K) \\ I_2(1) & \dots & I_2(K) \\ \vdots & \ddots & \vdots \\ I_N(1) & \dots & I_N(K) \end{bmatrix}}_{I_{\text{bus}}^K} = Y_{\text{bus}} \underbrace{\begin{bmatrix} V_1(1) & \dots & V_1(K) \\ V_2(1) & \dots & V_2(K) \\ \vdots & \ddots & \vdots \\ V_N(1) & \dots & V_N(K) \end{bmatrix}}_{V_{\text{bus}}^K}, \quad (2)$$

where V_{bus}^K and I_{bus}^K collect nodal voltages and injected currents sampled at K successive time slots (with white noise) by μ PMU installed downstream of the nodes in the primary distribution network (i.e., on subfeeders originating from them).

The iPF problem that we study in this paper concerns recovering the admittance matrix of a poly-phase distribution system, Y_{bus} , from voltage and current phasor measurements of all nodes, V_{bus}^K and I_{bus}^K . In general, V_{bus}^K is low rank in a power system making the identification problem ill-posed. This is reported for transmission PMU data in [19] and is further supported by the experiments on real μ PMU data obtained from [23]. In the following, we first study how the admittance matrix can be identified when the identification problem is well-posed. We discuss in Section IV how a large part of the admittance matrix can be identified despite the low rank structure of V_{bus}^K . We call the iPF problem *well-posed* when the measurement matrix V_{bus}^K has full rank, and call it *ill-posed* when V_{bus}^K is low rank.

B. Sparsity-based Regularization

This section presents a robust algorithm for recovering the admittance matrix of a distribution system from noisy sensor data. Existing synchrophasor technology is capable of sampling voltage and current waveforms at 120 Hz or higher [3]. But even at a lower temporal resolution (e.g., one-minute), enough data can be collected to identify the model of a distribution network comprised of several hundred nodes, before it changes. Nevertheless, for convenience, we henceforth refer to the available sensor data as μ PMU data. We make the following two assumptions: (a) the identification problem is well-posed, and (b) all nodes can be monitored.

The admittance matrix can be identified by solving the following regression problem:

$$\begin{aligned} \hat{Y}_{\text{bus}} &= \underset{Y}{\operatorname{argmin}} \|Y V_{\text{bus}}^K - I_{\text{bus}}^K\|_F \\ \text{subject to } & Y \in \mathbb{S}^{N \times N}. \end{aligned} \quad (3)$$

In practice, the sample size K can be smaller than the number of unknown variables in the admittance matrix and we seek for a sparse solution because Y_{bus} encodes the topology of a distribution network which is typically radial at any given time (hence, most elements of the admittance matrix are zero). Thus, we adopt sparsity-based regularization techniques to identify the admittance matrix. We specifically enforce sparsity

of Y_{bus} by applying the *vec* operator, which converts a matrix into a column vector, to the objective function and constraining the ℓ_0 -norm of $\operatorname{vec}(Y_{\text{bus}})$:

$$\begin{aligned} \hat{Y}_{\text{bus}} &= \underset{Y}{\operatorname{argmin}} \|((V_{\text{bus}}^K)^\top \otimes \mathbb{1}_N) \operatorname{vec}(Y) - \operatorname{vec}(I_{\text{bus}}^K)\|_2 \\ \text{subject to } & Y \in \mathbb{S}^{N \times N}, \quad \|\operatorname{vec}(Y)\|_0 \leq \delta, \end{aligned} \quad (4)$$

where \otimes is the Kronecker product and δ determines the degree of sparsity of Y_{bus} . The cardinality constraint makes this problem NP-hard [24].

Exploiting the symmetric structure of Y_{bus} , we reduce the number of parameters that need to be estimated. Consider a mapping $f: \mathbb{C}^{N \times N} \rightarrow \mathbb{C}^{(N^2+N)/2 \times 1}$ which collects the lower triangular elements of a complex matrix as illustrated below:

$$f(A) = [a_{11}, a_{21}, a_{31}, \dots, a_{N1}, a_{22}, a_{32}, \dots, a_{N2}, \dots, a_{NN}]^\top,$$

where a_{ij} is the element in the i th row and j th column of matrix A . Observe that f is a bijection for any $Y \in \mathbb{S}^{N \times N}$ and we have $\operatorname{vec}(Y) = Q_Y f(Y)$, where $Q_Y \in \mathbb{R}^{N^2 \times (N^2+N)/2}$ is a unique binary matrix that converts $f(Y)$ to $\operatorname{vec}(Y)$. Hence, the iPF problem can be reformulated as:

$$f(\hat{Y}) = \underset{x \in \mathbb{C}^{(N^2+N)/2 \times 1}}{\operatorname{argmin}} \left\| (V_{\text{bus}}^K)^\top \otimes \mathbb{1}_N \right\| Q_Y x - \operatorname{vec}(I_{\text{bus}}^K) \Big\|_2^2 + \lambda \|x\|_0,$$

where λ is a suitable positive regularization parameter. The above problem is non-convex and cannot be solved efficiently; thus, we solve a convex relaxation of this problem known as the lasso [25], hoping that the solutions coincide. In [9], conditions are established for the solution of ℓ_1 optimization to coincide with the solution of ℓ_0 optimization. The penalized form of lasso can be written as:

$$\min_{x \in \mathbb{C}^{(N^2+N)/2 \times 1}} \left\| \underbrace{\left((V_{\text{bus}}^K)^\top \otimes \mathbb{1}_N \right) Q_Y x}_{A} - \underbrace{\operatorname{vec}(I_{\text{bus}}^K)}_b \right\|_2^2 + \lambda \|x\|_1. \quad (5)$$

The lasso continuously shrinks the elements of Y_{bus} toward 0 as λ increases, and some coefficients are shrunk to exact 0 if λ is sufficiently large. Hence, selecting λ is critical to the performance of the lasso. One way to choose this regularization parameter is to minimize the Bayesian information criterion (BIC) as discussed in [14]. We note that (5) can be solved using a standard convex optimizer as well as iterative algorithms [26]–[28], which are more compelling in large distribution networks.

In practice, it may be possible to obtain partial information about the network topology. To improve the performance of the identification algorithm, this information can be incorporated in the form of equality constraints added to Eq. (5). In this paper, we consider a general situation where the network topology is unknown completely.

Once $f(\hat{Y})$ is recovered, $\operatorname{vec}(\hat{Y})$ can be easily constructed:

$$\operatorname{vec}(\hat{Y}) = Q_Y f(\hat{Y}). \quad (6)$$

It is shown in [7] that the proposed technique can solve the identification problem when it is well-posed.

C. Avoiding Unnecessary Bias

Despite significant statistical and computational advantages of the lasso for solving the iPF problem, it is not an ‘oracle procedure’ and could result in suboptimal estimation in certain cases [29]. The lasso equally penalizes all elements of Y_{bus} , thereby producing biased estimates for the large elements. Hence, it may fail to identify the true admittance matrix when the distribution system contains several switches and voltage regulators which have much larger admittance than the distribution lines.

To avoid the unnecessary bias, we can assign data-dependent weights to different elements of Y_{bus} in the ℓ_1 penalty. The two-stage algorithm, known as the adaptive lasso [29], applies less shrinkage whenever the true unknown variable is large. Specifically, $f(Y)$ can be recovered from:

$$\min_{x \in \mathbb{C}^{(N^2+N)/2 \times 1}} \|Ax - b\|_2^2 + \lambda \sum_i \frac{|x_i|}{|\hat{x}_i|^\gamma}, \quad (7)$$

where γ is a positive parameter and \hat{x}_i is an initial estimator for x_i , e.g., the ordinary least squares (OLS) estimator defined:

$$\hat{x} = (A^\top A)^{-1} A^\top b.$$

Rescaling the columns of $A = (V_{\text{bus}}^{K\top} \otimes \mathbb{1}_N) Q_Y$ with the corresponding weights, i.e., $|\hat{x}_i|^\gamma$, reduces (7) to the standard lasso problem, and therefore, it can be solved using the same algorithms developed for the lasso. Note that two-dimensional cross-validation is typically used to tune (λ, γ) .

In Section VI, we compare the lasso and the adaptive lasso penalties and show that the adaptive lasso outperforms the lasso in terms of identification accuracy in the test feeders.

D. Exploiting Additional Structure

Distribution circuits are upgraded and reconfigured to meet the growing demand of a neighbourhood, accommodate new technologies installed at customers’ premises, and minimize losses. These changes are seldom incorporated into the distribution system model; thus, the available model is usually obsolete and cannot be relied on for diagnostics and control applications. We now discuss how such an approximate model can be leveraged to improve the identification accuracy.

We represent the available (and presumably inaccurate) admittance matrix of a distribution system by $\tilde{Y} \triangleq Y_{\text{bus}} + \Psi$ where Y_{bus} is the true admittance matrix of the network, which we ultimately intend to find, and Ψ is an arbitrary error matrix that must be identified. We note that Ψ is symmetric since both \tilde{Y} and Y_{bus} are symmetric. If all elements of Ψ are small, the identification problem reduces to solving the following regularized least squares problem:

$$\hat{Y}_{\text{bus}} = \tilde{Y} - \underset{\Psi \in \mathbb{S}^{N \times N}}{\text{argmin}} \left\| (\tilde{Y} - \Psi) V_{\text{bus}}^K - I_{\text{bus}}^K \right\|_F^2 + \lambda \|\Psi\|_F^2, \quad (8)$$

where λ is a tuning parameter.

Alternately, Ψ might have a small number of nonzero elements that are not necessarily small, e.g., when the only unknown information is the status of switches which typically have large admittance values. In such cases, the Frobenius norm of Ψ in (8) must be replaced with the ℓ_0 -norm of Ψ and

similarly the ℓ_2 -norm of x in (9) must be replaced with its ℓ_1 -norm (after convex relaxation).

Exploiting the symmetric structure of Ψ and adopting the technique outlined in Section III-B, we can solve the following ridge regression problem to identify Ψ :

$$f(\hat{\Psi}) = \underset{x \in \mathbb{C}^{(N^2+N) \times 1}}{\text{argmin}} \|Ax - b\|_2^2 + \lambda \|x\|_2^2 \quad (9)$$

where $A = -(V_{\text{bus}}^{K\top} \otimes \mathbb{1}_N) Q_\Psi$ and $b = \text{vec}(I_{\text{bus}}^K - \tilde{Y} V_{\text{bus}}^K)$. This approach can be used to periodically update the distribution system model.

Remark 1. This problem can be solved analytically with a very high computational complexity, i.e., $\mathcal{O}(\text{cdim}(A)^3)$, where $\text{cdim}(A)$ denotes the number of columns in A . Alternatively, it is well-known that we can solve it using the standard gradient descent.

IV. LOW RANK STRUCTURE OF DISTRIBUTION SYSTEMS

The voltage measurement matrix, V_{bus}^K , is low rank in most poly-phase distribution systems due to the interdependencies between nodal voltages; this matrix has several singular values that are too small even when we consider the measurement error introduced by μ PMUs. This results in an ill-posed problem that cannot be solved to identify the admittance matrix in its entirety even if $K \gg N$. To tackle this problem, we propose a novel identification algorithm based on a particular partitioning of V_{bus}^K into two matrices, one of which has full row rank; this permits us to recover at least some part of the admittance matrix while the rest of it cannot be recovered. The steps of this algorithm are described below.

A. Similarity Transformation

Let R be the row rank of V_{bus}^K . We partition V_{bus}^K into two matrices via a similarity transformation of the matrix Y_{bus} :

$$\underbrace{\mathcal{T} I_{\text{bus}}^K}_{\mathbb{I}} = \underbrace{(\mathcal{T} Y_{\text{bus}} \mathcal{T}^{-1})}_{\mathbb{Y}} \underbrace{(\mathcal{T} V_{\text{bus}}^K)}_{\mathbb{V}}, \quad (10)$$

where \mathcal{T} is a $\sum_{n \in \mathcal{N}} |\mathcal{P}_n| \times \sum_{n \in \mathcal{N}} |\mathcal{P}_n|$ matrix that splits V_{bus}^K into an $R \times K$ matrix, denoted by \mathbb{V}_2 , containing R linearly independent rows of V_{bus}^K and an $(\sum_{n \in \mathcal{N}} |\mathcal{P}_n| - R) \times K$ matrix, denoted by \mathbb{V}_1 , containing other rows of V_{bus}^K that are all in the row space of \mathbb{V}_2 . Algorithm 1 describes the steps for building these two submatrices from the available synchrophasor data. Shuffling rows of V_{bus}^K and I_{bus}^K according to this transformation yields:

$$\mathcal{T} V_{\text{bus}}^K = \begin{bmatrix} \mathbb{V}_1 \\ \mathbb{V}_2 \end{bmatrix}, \quad \mathcal{T} I_{\text{bus}}^K = \begin{bmatrix} \mathbb{I}_1 \\ \mathbb{I}_2 \end{bmatrix}.$$

Since \mathbb{V}_1 is in the row space of \mathbb{V}_2 , we can estimate the basis X such that $\mathbb{V}_1 = X \mathbb{V}_2$ from μ PMU data by computing the pseudo-inverse of \mathbb{V}_2 : $X = \mathbb{V}_1 \mathbb{V}_2^\dagger$. Note that the pseudo-inverse is well-defined here since \mathbb{V}_2 is full row rank.

B. Recovering Parts of Y_{bus}

We write (10) as

$$\begin{bmatrix} \mathbb{I}_1 \\ \mathbb{I}_2 \end{bmatrix} = \underbrace{\begin{bmatrix} \mathbb{Y}_{1,1} & \mathbb{Y}_{1,2} \\ \mathbb{Y}_{2,1} & \mathbb{Y}_{2,2} \end{bmatrix}}_{\mathbb{Y}} \begin{bmatrix} X \mathbb{V}_2 \\ \mathbb{V}_2 \end{bmatrix} = \begin{bmatrix} \mathbb{Y}_{1,1} X + \mathbb{Y}_{1,2} \\ \mathbb{Y}_{2,1} X + \mathbb{Y}_{2,2} \end{bmatrix} \mathbb{V}_2, \quad (11)$$

Algorithm 1 Basis Selection Algorithm

- 1: Perform orthogonal-triangular decomposition of V_{bus}^K ;
 - 2: Sort diagonal elements of the upper triangular matrix;
 - 3: Choose the first R elements; return the corresponding elements in the permutation matrix as indices of the linearly independent rows of V_{bus}^K ;
-

where $\{\mathbb{Y}_{i,j}\}_{i,j \in \{1,2\}}$ are four submatrices of \mathbb{Y} obtained according to the decomposition of \mathbb{V} . Note that \mathbb{V}_2 has full row rank. We have

$$\mathbb{I}_1 = (\mathbb{Y}_{1,1}X + \mathbb{Y}_{1,2})\mathbb{V}_2, \quad (12)$$

$$\mathbb{I}_2 = (\mathbb{Y}_{1,2}^\top X + \mathbb{Y}_{2,2})\mathbb{V}_2. \quad (13)$$

Solving (12) for $\mathbb{Y}_{1,2}$ and substituting it into (13) yields:

$$-X^\top \mathbb{Y}_{1,1}X + \mathbb{Y}_{2,2} = C, \quad (14)$$

in which $C = \mathbb{I}_2 \mathbb{V}_2^\dagger - (\mathbb{V}_2^\dagger)^\top \mathbb{I}_1^\top X$ can be computed from the μ PMU data. Vectorizing both sides of the equation yields:

$$-(X^\top \otimes X^\top) \text{vec}(\mathbb{Y}_{1,1}) + \text{vec}(\mathbb{Y}_{2,2}) = \text{vec}(C).$$

This problem can be written in the following form to reduce the number of parameters that need to be estimated using bijection f and matrix Q :

$$-(X^\top \otimes X^\top) Q_{Y_{11}} f(\mathbb{Y}_{1,1}) + Q_{Y_{22}} f(\mathbb{Y}_{2,2}) = \text{vec}(C).$$

Enforcing sparsity of the components of Y_{bus} , it is possible to identify $\mathbb{Y}_{1,1}$ and $\mathbb{Y}_{2,2}$ from this optimization problem:

$$\begin{aligned} \begin{bmatrix} f(\widehat{\mathbb{Y}}_{1,1}) \\ f(\widehat{\mathbb{Y}}_{2,2}) \end{bmatrix} &= \arg \min_x \lambda \sum_i w_i |x_i| + \\ &\|[-(X^\top \otimes X^\top) Q_{Y_{11}}, Q_{Y_{22}}] x - \text{vec}(C)\|_2^2. \end{aligned} \quad (15)$$

Depending on whether we use the lasso or the adaptive lasso penalty, w_i is set to 1 or $1/|\hat{x}_i|^\gamma$ for some $\gamma > 0$.

Once this problem is solved, $\mathbb{Y}_{1,2}$ can be identified from (13) using the method of least squares. However, there is no guarantee that $\mathbb{Y}_{1,2}$ is estimated with sufficient accuracy as the error introduced in the process of estimating $\mathbb{Y}_{2,2}$ propagates. We show in Section VI that $\mathbb{Y}_{2,2}$ can be accurately estimated in all cases despite the low rank structure, while $\mathbb{Y}_{1,1}$ and $\mathbb{Y}_{1,2}$ cannot be recovered with sufficient accuracy.

V. TIMELY DETECTION AND LOCALIZATION OF EVENTS

Several types of power system events, such as switching actions, tap operations, arc and ground faults can change the effective admittance between the nodes, thereby resulting in a different admittance matrix. In this section, we propose an online algorithm for tracking changes in the admittance matrix of a distribution system and identifying the events that induced these changes. This algorithm requires a small amount of data and has a low false alarm rate, enabling operators to take remedial actions in quasi real-time.

Consider an affine parameterization of the admittance matrix, denoted by $Y_{\text{bus}}^{\delta(k)}$, where

$$\delta(k) = \begin{cases} 0, & k < t \\ 1, & k \geq t \end{cases}$$

is the discrete mode and t is the time that the event has occurred. Our goal is to determine t and find out how the admittance matrix has changed by estimating $Y_{\text{bus}}^1 - Y_{\text{bus}}^0$ using as few successive voltage and current phasor measurements as possible. The updated entries of the admittance matrix indicate the type and approximate location of the event. For instance, if two elements of the admittance matrix change in a certain way during an event, it can be attributed to a switch that was opened while another one was closed.

A. Event Detection

To detect a change in the admittance matrix, we estimate the injected current vector at time k from Ohm's law using the known admittance matrix, Y_{bus}^0 , and the measured voltage vector at time k . We then compare the estimated injected current vector \hat{I}_{bus} with the measured current vector I_{bus} at time k to calculate the prediction error:

$$e(k) = I_{\text{bus}}(k) - \hat{I}_{\text{bus}}(k) = I_{\text{bus}}(k) - Y_{\text{bus}}^0 V_{\text{bus}}(k). \quad (16)$$

The series $e(\cdot)$ is white noise if the admittance matrix does not change; this can be verified by the turning point test. For a detailed discussion on how network topology errors can be detected, the readers can refer to [30]. When the prediction error $\|e(k)\|$ exceeds a predefined threshold, we assert that the admittance matrix has changed at time k .

B. Event Localization

The simplest approach to event localization is to run the identification algorithm presented in the previous section upon detection of an event to update the admittance matrix. In a large distribution system, this requires collecting and processing a considerable number of μ PMU samples following the detection, implying that the identification task may not be accomplished in a timely manner. To address this shortcoming, we propose an identification algorithm that scales with the size of the network by taking advantage of the knowledge of the admittance matrix before an event and the fact that only a small number of its elements will change during the event.

Given that the effective admittance between just a small number of nodes is expected to change in an event, the difference between the two admittance matrices corresponding to the systems before and after the event must be sparse. We leverage this sparsity to recover the new admittance matrix:

$$\begin{aligned} \min_{Y_{\text{bus}}^1} & \| \text{vec}(Y_{\text{bus}}^1 - Y_{\text{bus}}^0) \|_0 \\ \text{subject to} & \quad I_{\text{bus}}^{t \rightarrow t+K} = Y_{\text{bus}}^1 V_{\text{bus}}^{t \rightarrow t+K} \\ & \quad Y_{\text{bus}}^1 \in \mathbb{S}_{\sum_{n \in \mathcal{N}} |\mathcal{P}_n| \times \sum_{n \in \mathcal{N}} |\mathcal{P}_n|}, \end{aligned} \quad (17)$$

in which Y_{bus}^0 is known, t is the time slot when the event is detected, and

$$I_{\text{bus}}^{t \rightarrow t+K} = \begin{bmatrix} I_1(t) & \dots & I_1(t+K) \\ I_2(t) & \dots & I_2(t+K) \\ \vdots & \ddots & \vdots \\ I_N(t) & \dots & I_N(t+K) \end{bmatrix},$$

TABLE I
PROPERTIES OF THE RADIAL TEST FEEDERS.

feeder	no. nodes	$\text{rank}(V_{\text{bus}}^K)$	sparsity level	$ \max(Y_{\text{bus}}) $
13-bus	35	27	81.63%	10^7
34-bus	95	84	91.72%	402.1
37-bus	117	109	92.47%	1012.5
123-bus	275	254	97.39%	10^6

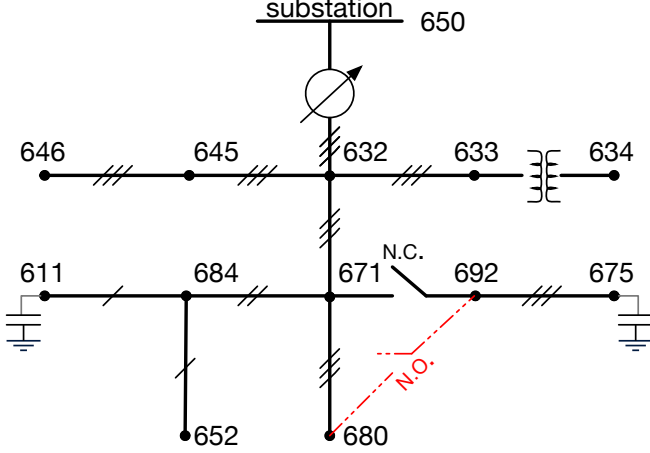


Fig. 2. A one-line diagram of the modified IEEE 13-bus test feeder. The dashed line represents the switch added to the original feeder. The number of phases connecting two nodes is shown by slashes on the lines.

modify this system by adding a normally open switch with the exact same configuration between Bus 680 and Bus 692 as shown in Figure 2. This creates two feasible radial structures that span all nodes. We use this feeder to validate both event detection and system identification algorithms. The 34-bus and 37-bus feeders do not have a switch and are merely used for the purpose of validating the identification algorithm.

B. Residential Loads & Phasor Measurements

A node in the distribution system model represents an aggregation point where usually a pole-top transformer supplies a small number of residential customers. Since distribution circuits are not modelled beyond these transformers, we aggregate demands of downstream customers at the corresponding nodes. We assume that each node is monitored by a μ PMU which measures the magnitude and phase angle of the node voltage and the current drawn by the downstream customers once every time slot.

We use real data from the ADRES dataset [35] to model the customers connected to the 13-bus, 34-bus, and 37-bus test feeders. This dataset consists of high-resolution (1 second) measurements of real power, reactive power, and per-phase voltage values of 30 Austrian households over 14 days. To obtain a sufficient number of customers for our simulation, we treat a 3-phase load as three separate single-phase loads, and split 14 days of available data for each household into 14 individual loads each representing the demand of a customer over a particular day. We connect a random number of customers between 5 and 15 to each node, except the nodes that are terminals of voltage regulators and switches; no load is connected to these nodes.

TABLE II
ESTIMATION ERROR OF $\hat{Y}_{2,2}$ BY THE LASSO AND ADAPTIVE LASSO.

feeder	lasso		adaptive lasso	
	M1	M2	M1	M2
13-bus (radial)	5.51	4.71	3.88	1.76
13-bus (non-radial)	5.38	4.71	3.81	1.77
34-bus	243.65	18.84	21.47	9.11
37-bus	28.70	8.09	2.71	1.63

In the case of the IEEE 123-bus feeder, we need high-resolution measurements of many households, which we lack. To address this problem, we synthesize residential loads (real power) using the continuous-time Markov models derived from fine-grained measurements of the power consumption of 20 households in Ontario [36]. We connect a random number of customers between 5 and 10 to each node, except the nodes that represent the terminals of voltage regulators and switches. Hence, the load distribution is nonuniform across different phases of a node. We consider a constant power factor of 95% at each node, which is typical for residential loads, and set the reactive power accordingly in each time slot.

C. Results

To deal with the low rank structure of the test feeders, we utilize the algorithm proposed in Section IV to identify the largest part of the admittance matrix that could be possibly recovered from the available data. We also utilize the event detection and localization algorithm proposed in Section V to track how the admittance matrix changes in an event. To validate these algorithms, we perform several simulation runs for each test feeder where each simulation spans one day divided into 1-second time slots. In each case, we estimate the admittance matrix using both the lasso and the adaptive lasso penalties and compare their performance. We use two metrics to quantify the error incurred in estimating $\hat{Y}_{2,2}$, which is a submatrix of \hat{Y} that excludes the rows and columns corresponding to the primary side of the voltage regulator and the distribution transformer (i.e., Bus 633):

$$\text{Metric 1 (M1): } \|\text{vec}(\hat{Y}_{2,2} - Y_{2,2})\|_1$$

$$\text{Metric 2 (M2): } \|\hat{Y}_{2,2} - Y_{2,2}\|_F$$

Metric M1 is used to evaluate the error of topology identification, while Metric M2 is the error of parameter estimation.

To tune the parameters of the convex programs, we search through a reasonable set of values. Specifically, γ and λ of the adaptive lasso are chosen from $\{0.5, 1, 2\}$ and the set of logarithmically spaced points between 10^5 and 10^{-5} , respectively. The same set of values are considered to determine λ of the lasso. Moreover, the OLS estimator is adopted as the weight of the ℓ_1 penalty in the adaptive lasso.

1) *Identification with Precise Measurements:* We first explore the scenario in which μ PMU measurements are not affected by noise. Table II shows the two error metrics when the lasso or the adaptive lasso penalty is used to identify the admittance matrix of the three test feeders. In the case of the 13-bus feeder, both methods can detect the true topology of the network and estimate all elements of $\hat{Y}_{2,2}$ except one, with less than 1% relative error. The one element that is not accurately identified corresponds to the substation. Nevertheless, the adaptive lasso estimates that element with

a lower error compared to the lasso as suggested by the two error metrics representing the overall accuracy of these methods. Should we leverage the knowledge of the substation type and configuration, both methods can accurately estimate all elements of $\hat{\mathbf{Y}}_{2,2}$ ($M1, M2 < 0.01$).

We next validate our method on a mesh network by adding a single-phase line between Bus 611.3 and Bus 646.3. Table II shows that our algorithm can identify the topology and parameters except for one element that corresponds to the substation. Similar to the previous case, the adaptive lasso estimates that element more accurately than the lasso as suggested by the two error metrics.

In the case of the 34-bus and 37-bus feeders, the lasso fails to accurately identify more than one element of the admittance matrix, resulting in estimation errors which are remarkably higher than the previous case. We verify that those elements have large admittance values. However, the adaptive lasso successfully estimates those elements in both feeders and detects the true topology of the network, resulting in relatively smaller estimation errors.

2) *Identification with Noisy Measurements:* We now explore the scenario in which μ PMU measurements are noisy. We only show the results for the 13-bus feeder due to space limitations. To simulate the measurement error, we add a white Gaussian noise with zero mean and variance σ^2 to node voltages and treat them as μ PMU measurements under the assumption that the instrumental transformers are calibrated according to the data sheets. We have observed that perturbing node voltages by a small Gaussian noise does not completely eliminate the low rank problem for smaller feeders such as the IEEE 13-bus network. We try different values of σ and perform ten simulation runs for each value. In particular, we increase the standard deviation from 10^{-6} to 10^{-2} and report the mean value of the two error metrics over these runs. Figure 3 shows the mean estimation error of the lasso and the adaptive lasso. It can be seen that both methods are quite sensitive to noise. When $\sigma = 10^{-6}$, the estimation error of both methods is quite similar to the scenario with precise measurements (see Table II). The adaptive lasso can accurately identify all elements of $\hat{\mathbf{Y}}_{2,2}$, except for one element (as discussed earlier) as long as $\sigma \leq 10^{-3}$. Should σ exceeds this level, the adaptive lasso fails to identify several elements and both error metrics increase significantly. This is because the noise standard deviation of around 10^{-2} is quite large for the line impedance values, making the identification problem impossible to solve. Unlike the adaptive lasso, the lasso is less robust to noise and only yields sufficiently accurate estimates when $\sigma \leq 10^{-4}$.

3) *Event Detection and Localization:* We finally validate the proposed event detection and localization algorithm by simulating a line tripping event and a switching operation in the 13-bus test feeder, and a switching operation in the 123-bus test feeder. These events are triggered after the admittance matrix has been identified for the initial configuration of the distribution system.

We first focus on the 13-bus test feeder. We introduce a line tripping event by disconnecting the single-phase line between Bus 611 and Bus 684, and a switching event by closing the switch between Bus 692 and Bus 680 while opening the switch between Bus 671 and Bus 692. Both events will change the

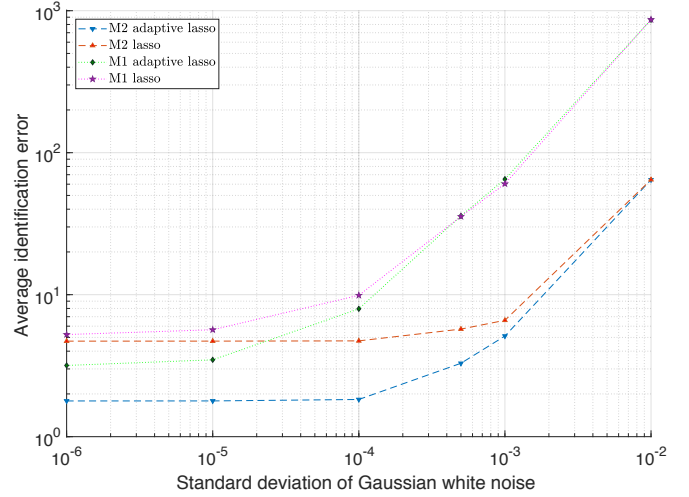


Fig. 3. Identification error of the lasso and the adaptive lasso for different noise levels in the IEEE 13-bus test feeder.

admittance matrix and therefore must be identifiable from the available data. We observe that the proposed algorithm detects the event in both cases in the same time slot that it occurs, i.e., immediately after processing the μ PMU data for that time slot. For the switching event, $\Delta\hat{\mathbf{Y}}$ can be estimated with relatively high accuracy ($M1 = 0.17, M2 = 0.10$) using 23 μ PMU samples following the detection of this event, as shown in Figure 4. In this figure, the color of a cell located at row i and column j represents the value of $|\hat{\mathbf{Y}}^1(i, j) - \hat{\mathbf{Y}}^0(i, j)|$. It can be readily seen that all elements of $\Delta\hat{\mathbf{Y}}$ are zero except for 6 three by three submatrices which have changed due to this event, enabling us to locate the event within a small geographical area. We verified that these submatrices correspond to the admittance of the two switches that are operated. Note that these switches are located on three-phase lines. The estimation error will increase significantly if we use fewer samples to identify $\Delta\hat{\mathbf{Y}}$.

Turning our attention to the 123-bus test feeder, we simulate a line switching event by closing the switch between Bus 13 and Bus 152 while opening the switch between Bus 151 and Bus 300 (refer to [37] for the topology of this feeder). The simultaneous switching operation maintains the radial structure of this distribution system. The proposed algorithm detects the event in the same time slot that it occurs and accurately identifies $\Delta\hat{\mathbf{Y}}$ ($M1, M2 < 0.1$) using a small number of μ PMU samples following the detection.

VII. CONCLUSIONS

Widespread adoption of distributed energy resources in power distribution grids calls for an advanced operation paradigm centered around monitoring, diagnostics, and control. While the knowledge of the distribution system model is crucial for most diagnostics and control applications, this model is often unavailable or outdated in practice. This paper explored how the admittance matrix of a poly-phase power distribution system can be identified from limited voltage and current phasor measurements of inexpensive distribution PMUs. We proposed tractable convex programs to recover the admittance matrix in various settings and to track changes

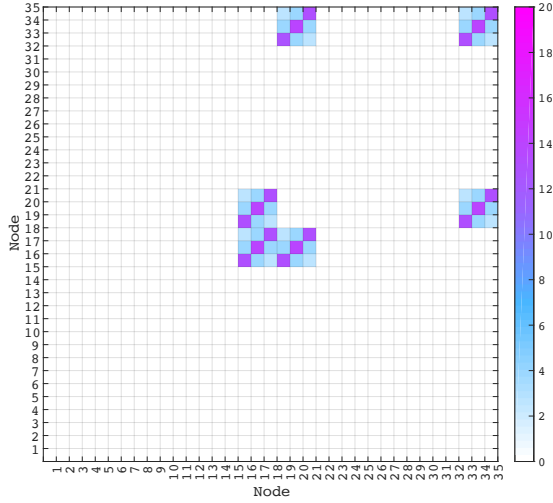


Fig. 4. A colored representation of $\Delta\hat{Y}$ when 23 μ PMU samples are used to recover the admittance matrix following the detection of the switching event.

in the network topology, and investigated the fundamental limitations of these techniques. We showed that the network topology can be accurately determined in all test networks, and the parameters of a reduced admittance matrix can be estimated with sufficient accuracy as long as the measurement error is below a certain level.

There are several avenues for future work. The μ PMU installation is currently limited in low-voltage distribution networks. Furthermore, μ PMUs occasionally send corrupt data that is not suitable for identification. To address these problems, we intend to develop techniques that leverage both smart meter and μ PMU data to improve identifiability of low-voltage distribution grids. We also plan to develop an identification algorithm that can deal with hidden states in the network. Moreover, the proposed technique can be computationally expensive and sensitive to noise when it is applied to a distribution network with noisy measurements from thousands of nodes. We intend to develop a robust distributed identification algorithm for large distribution networks.

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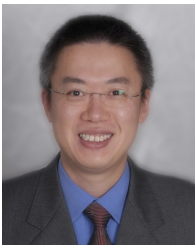
Omid Ardakanian (M'15) received the B.Sc. degree in Computer Engineering from Sharif University of Technology, Iran, in 2009, and the M.Math and Ph.D. degrees in Computer Science from the University of Waterloo, Canada in 2011 and 2015, respectively. He was subsequently an NSERC postdoctoral fellow at the University of California at Berkeley, and the University of British Columbia. He joined the Department of Computing Science at the University of Alberta in 2017 and is currently an Assistant Professor. His research interests are in

the areas of computer networks, ubiquitous computing, and cyber-physical systems. He is currently the Information Services Director of ACM Emerging Interest Group on Energy Systems and Informatics, and a Guest Editor of *IEEE Transactions on Smart Grid* Special Issue on Theory and Application of PMUs in Power Distribution Systems. He has received best paper awards from IEEE PES General Meeting, ACM BuildSys, and ACM e-Energy.



Ye Yuan (M'13) received the B.Eng. degree (Valedictorian) from the Department of Automation, Shanghai Jiao Tong University, Shanghai, China, in September 2008, and the M.Phil. and Ph.D. degrees from the Department of Engineering, University of Cambridge, Cambridge, U.K., in October 2009 and February 2012, respectively. He is currently a Full Professor at the Huazhong University of Science and Technology, Wuhan, China. He was a Postdoctoral Researcher at UC Berkeley, a Junior Research Fellow at Darwin College, University of Cambridge,

and has been holding visiting researcher positions at California Institute of Technology, Massachusetts Institute of Technology, and Imperial College London. His research interests include system identification and control with applications to cyber-physical systems. Dr. Yuan has received the China National Recruitment Program of 1000 Talented Young Scholars, the Dorothy Hodgkin Postgraduate Award, Microsoft Research Ph.D. Scholarship.



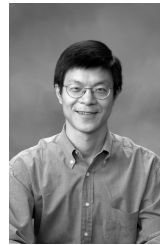
Vincent W.S. Wong (S'94, M'00, SM'07, F'16) received the B.Sc. degree from the University of Manitoba, Winnipeg, MB, Canada, in 1994, the M.A.Sc. degree from the University of Waterloo, Waterloo, ON, Canada, in 1996, and the Ph.D. degree from the University of British Columbia (UBC), Vancouver, BC, Canada, in 2000. From 2000 to 2001, he worked as a systems engineer at PMC-Sierra Inc. (now Microchip Technology Inc.). He joined the Department of Electrical and Computer Engineering at UBC in 2002 and is currently a Professor. His

research areas include protocol design, optimization, and resource management of communication networks, with applications to wireless networks, smart grid, mobile edge computing, and Internet of Things. Currently, Dr. Wong is an Executive Editorial Committee Member of *IEEE Transactions on Wireless Communications*, an Editor-at-Large of *IEEE Transactions on Communications*, and an Associate Editor of *IEEE Transactions on Mobile Computing*. He has served as a Guest Editor of *IEEE Journal on Selected Areas in Communications* and *IEEE Wireless Communications*. He has also served on the editorial boards of *IEEE Transactions on Vehicular Technology* and *Journal of Communications and Networks*. He is a Tutorial Co-Chair of *IEEE Globecom*'18. He was a Technical Program Co-chair of *IEEE SmartGridComm*'14, as well as a Symposium Co-chair of *IEEE ICC*'18, *IEEE SmartGridComm* ('13, '17) and *IEEE Globecom*'13. He is the Chair of the IEEE Vancouver Joint Communications Chapter and has served as the Chair of the IEEE Communications Society Emerging Technical Sub-Committee on Smart Grid Communications. He received the 2014 UBC Killam Faculty Research Fellowship.



Roel Dobbe is a Postdoctoral Researcher with the AI Now Institute at New York university, where he researches the social and political implications of artificial intelligence and automated decision-making. In 2018, Roel obtained a PhD in Control, Intelligent Systems & Energy from the Department of Electrical Engineering & Computer Sciences at UC Berkeley. He received a BS in Mechanical Engineering in 2007 and a MS in Systems & Control in 2010 from Delft University of Technology. His PhD research

focused on the design, analysis and integration of novel monitoring and control strategies for safetycritical systems, including in cancer research and electrical power systems. Roel's work on state estimation and machine learning for electric grid control has been developed with Lawrence Berkeley National Labs and was implemented on the Dutch national grid by utility Alliander. Roel also developed techniques to improve the interpretability and trust in machine learning algorithms used by utilities as a data scientist with C3 IoT in Silicon Valley.



Steven H. Low (F'00) is the Gilloon Professor of the Department of Computing & Mathematical Sciences and the Department of Electrical Engineering and has been with Caltech since 2000. Before that, he was with AT&T Bell Laboratories, Murray Hill, NJ from 1992 to 1996, and with the University of Melbourne, Australia from 1996 to 2000. He has been a co-recipient of IEEE best paper awards, on the editorial boards of major journals in networking and power systems, and Honorary/Chair professors in Australia, China and Taiwan. His research on

communication networks was accelerating more than 1TB of Internet traffic every second since 2014. He was a member of the Networking and Information Technology Technical Advisory Group for the US President's Council of Advisors on Science and Technology (PCAST) in 2006. He received his B.S. from Cornell and PhD from Berkeley, both in EE.



Alexandra von Meier (M'10) is an Associate Professor in the Dept. of Electrical Engineering and Computer Science, and Director of Electric Grid Research at the California Institute for Energy and Environment, at U.C. Berkeley. She was previously a Professor of Energy Management and Design at Sonoma State University. She holds a BA in Physics and a PhD in Energy and Resources from U.C. Berkeley.



Claire Tomlin (F'10) is the Charles A. Desoer Professor of Engineering in Electrical Engineering and Computer Sciences at the University of California, Berkeley. She was an Assistant, Associate, and Full Professor in Aeronautics and Astronautics at Stanford from 1998 to 2007, and in 2005 joined Berkeley. Claire works in the area of control theory and hybrid systems, with applications to air traffic management, UAV systems, energy, robotics, and systems biology. She is a MacArthur Foundation Fellow (2006) and an IEEE Fellow (2010), and in

2010 held the Tage Erlander Professorship of the Swedish Research Council at KTH in Stockholm.